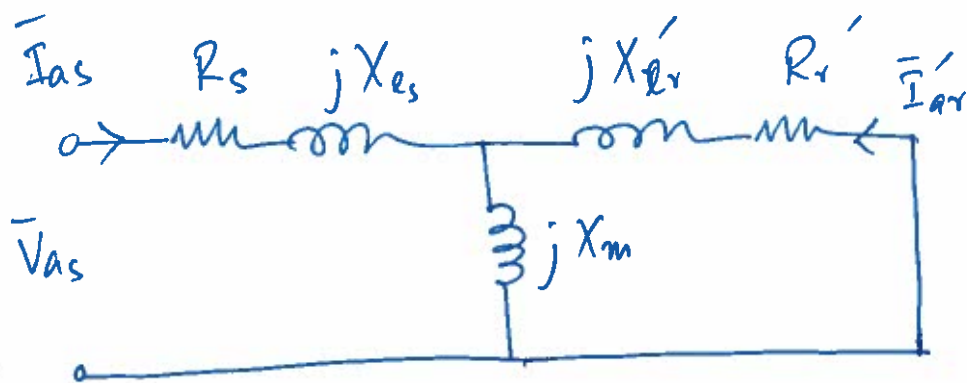




R_s = Resistance of stator

$\frac{R_r'}{s}$ = Resistance of rotor referred to stator
slip

X_{ls} = Leakage reactance of stator

X_{lr}' = Leakage reactance of rotor referred to stator.

X_m = Magnetizing reactance.

$\bar{V}_{as}$ = Terminal voltage phasor across phase a

$\bar{I}_{as}$ = Current entering phase a in the stator

multiplied by $e^{j(\text{same angle})}$.

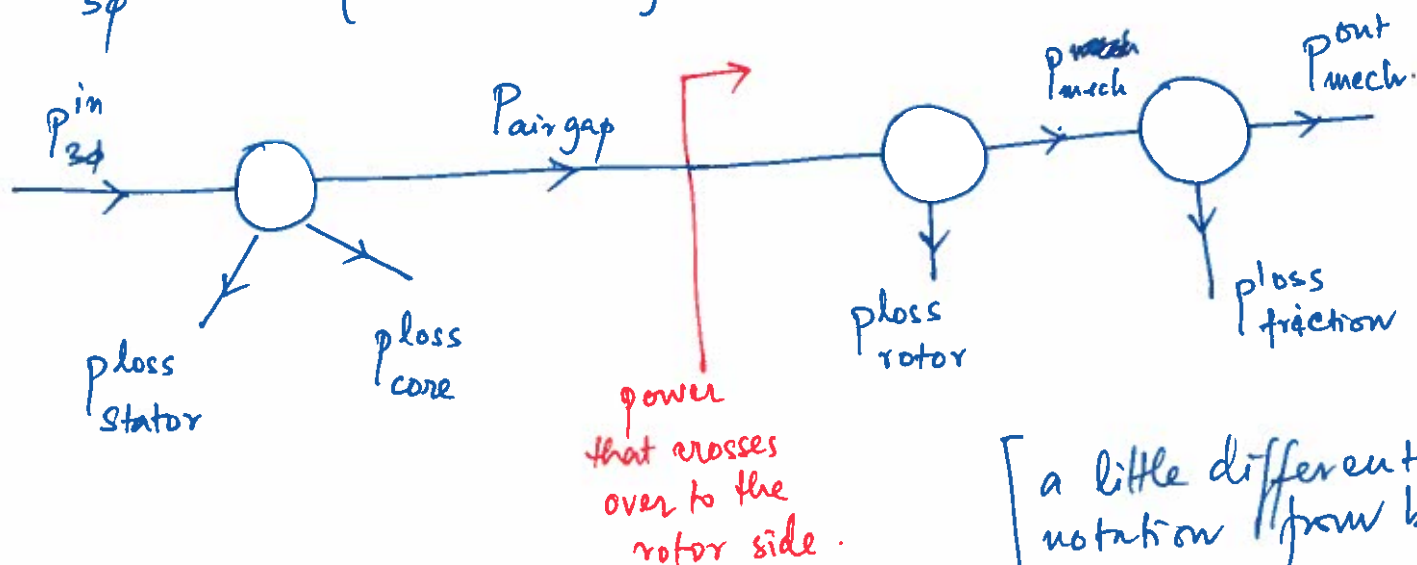
$\bar{I}_{ar}'$ = Rotor current phasor "rotated" and referred to the stator.

Agenda :

- ① Power and torque calculations
- ② Torque-slip curve.
- ③ Approximate circuit equivalent.

① Power and torque calculations.

$$P_{3\phi}^{in} = \operatorname{Re} \{ 3 \bar{V}_{as} \bar{I}_{as}^* \}.$$

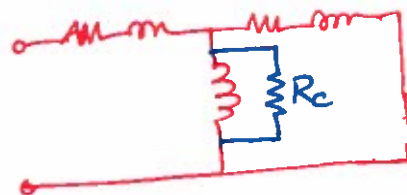


[a little different notation from book].

$$P_{\text{loss stator}} \left(\text{often written as } P_{sc} \right) = 3 \cdot |\bar{I}_{as}|^2 \cdot R_s$$

$$P_{\text{loss core}} \left(\text{often " " } P_c \right)$$

due to hysteresis and eddy currents



Recall transformers!

$$P_{\text{air gap}} \left(\text{often " " } P_{ag} \right)$$

$$P_{\text{loss rotor}} \left(\text{often " " } P_{rcl} \right) = 3 |\bar{I}_{ar}|^2 \cdot R_r$$

or P_r

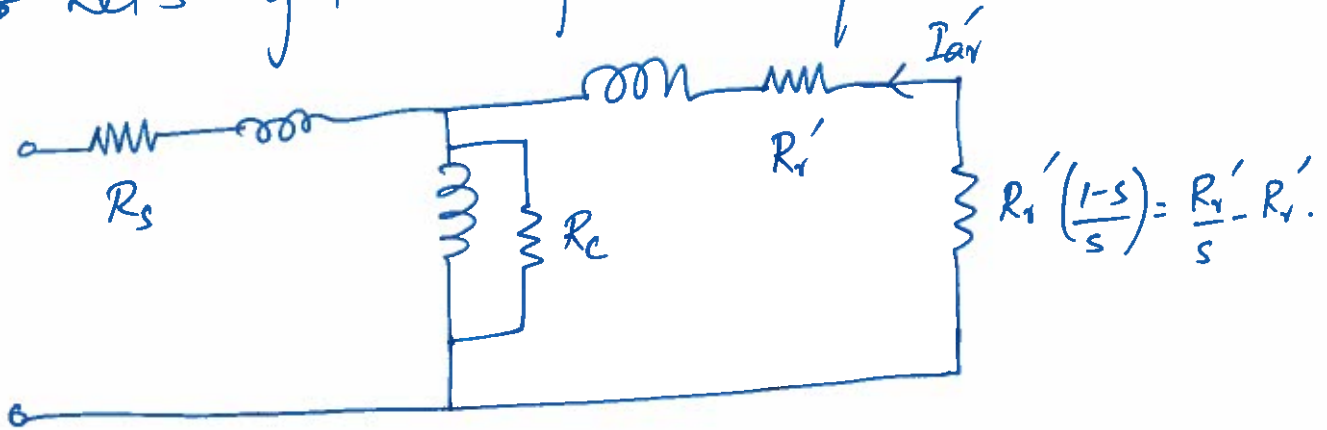
$$P_{\text{loss friction}} \left(\text{often " " } P_{rot} \right)$$

is specified directly.

$$P_{\text{mech}} \left(\text{often " " } P_m \right) = \text{amount of mechanical power developed.}$$

$$P_{\text{out mech}} \left(\text{often " " } P_{\text{out}} \right) = \text{useful shaft torque.}$$

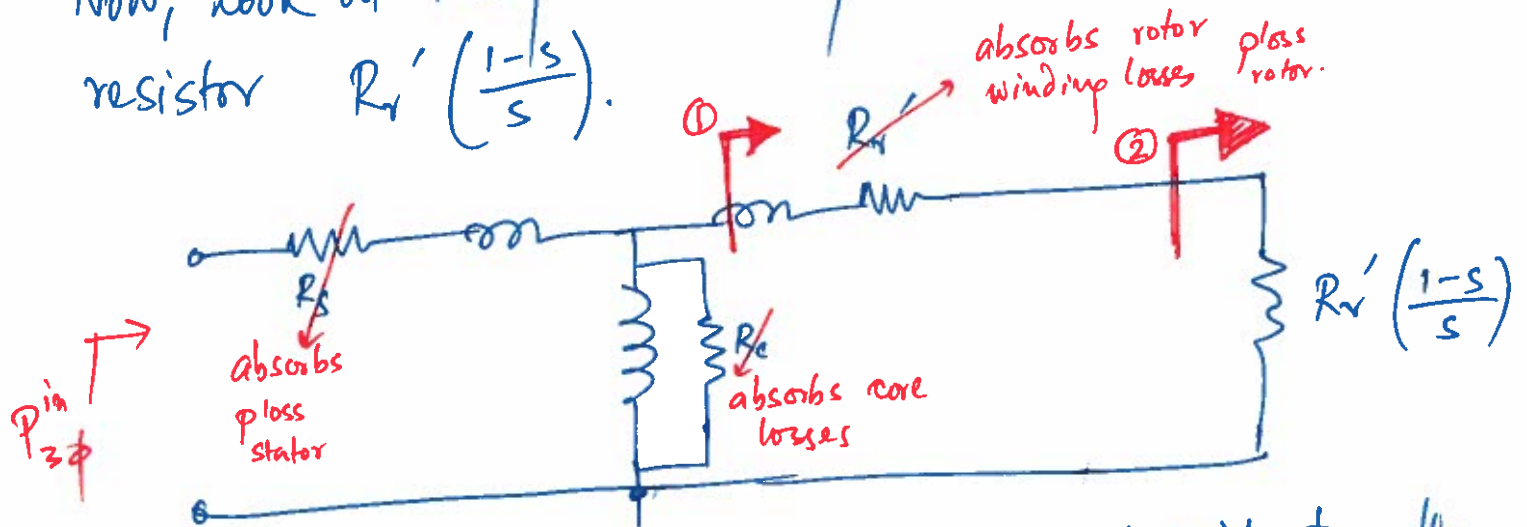
$P_{\text{air gap}} \div$ Let's get this from the equiv. crt.



NOTICE:



Now, look at the power dissipated across the resistor $R_r' \left(\frac{1-s}{s} \right)$.



Q. What's the power absorbed by the circuit to the right of the arrows at ① and ②?

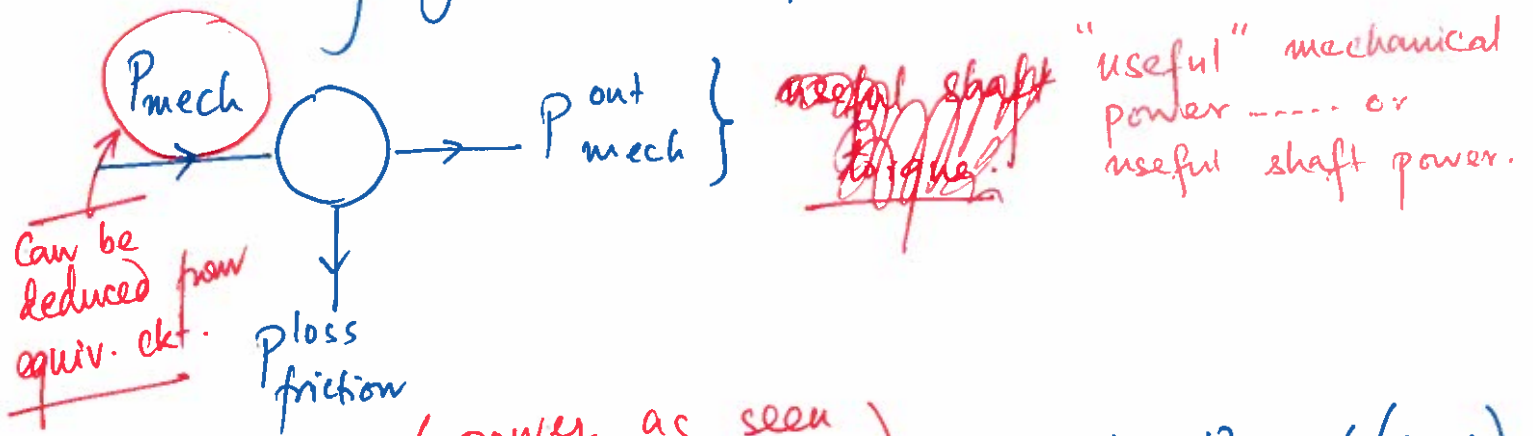
$$= P_{\text{in } 3\phi} - P_{\text{stator}}^{\text{loss}} - P_{\text{core}}^{\text{loss}}$$

$$= P_{\text{air-gap}}$$

$$= P_{\text{air-gap}} - P_{\text{rotor}}^{\text{loss}} = P_{\text{mech.}}$$

If there's no frictional losses, $P_{\text{mech}} = P_{\text{mech.}}^{\text{out}}$

Circuit only gives us info about P_{mech} .



$$* P_{mech} = \left(\begin{array}{l} \text{power as seen} \\ \text{from the arrow} \\ \text{marked with ②} \end{array} \right) = 3 \cdot |\bar{I}_{ar}'|^2 \cdot R_r' \left(\frac{1-s}{s} \right).$$

$$* P_{air-gap} = \left(\begin{array}{l} \text{power as seen} \\ \text{from arrow marked} \\ \text{as ①} \end{array} \right) = 3 \cdot |\bar{I}_{ar}'|^2 \cdot \frac{R_r'}{s}.$$

$$\therefore * P_{air-gap} = \frac{P_{mech}}{1-s}$$

How to compute T^e ?

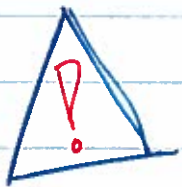
$$* T^e \cdot \omega_m = P_{mech}, \text{ and } \omega_m = (1-s) \omega_s.$$

$$\text{Also } \therefore T^e = \frac{P_{mech}}{\omega_m} = \frac{P_{mech}}{(1-s) \omega_s}$$

$$\text{Also } \dots P_{mech} = P_{air-gap} \cdot (1-s) \\ \Rightarrow T^e = \frac{P_{air-gap}}{\omega_s}.$$

All calculations done so far are for 2-pole machines...

For p -pole machines, $\frac{p}{2} \omega_m = (1-s) \omega_s$ or $\omega_s - \omega_r = \frac{p}{2} \omega_m$



$T^e \omega_m = P_{mech}$ always holds.

Only the relation between ω_m and ω_s changes when $p > 2$.

Example: A ^{3 ϕ} induction motor has 4-poles, runs on 60 Hz, 120 V (line-neutral) balanced 3 ϕ input. Its characteristic quantities referred to the stator are given by

$$R_s = 0, X_{ls} = 0, X_m = 40 \Omega, X_{lr}' = 1 \Omega, R_r' = 1.3 \Omega,$$

~~Assume~~ Neglect core and frictional losses. Suppose the rotor speed is given by 1720 RPM.

Find s , ω_r , $|I_{ar}'|$, P_{mech} , T^e , $P_{3\phi}^{in}$, $P_{air-gap}$, power factor of the motor, efficiency of the motor.

In tests, we shall provide you with the terms and not just symbols.

Let's dissect the problem / statement.

$$\underline{60 \text{ Hz}} \Rightarrow \omega_s = 2\pi \cdot 60 \text{ rad/s} \\ = 377 \text{ rad/s.}$$

$$\underline{120 \text{ V}} \text{ (line-neutral)} \Rightarrow |\bar{V}_{as}| = 120 \text{ V.}$$

You can always assume one angle in the ckt as a reference. Choose $\angle \bar{V}_{as} = 0^\circ$.
 $\therefore \bar{V}_{as} = 120 \angle 0^\circ \text{ Volts.}$

$$\underline{4\text{-poles}} \Rightarrow p = 4 \Rightarrow \omega_m \cdot \frac{p}{2} = \omega_s - \omega_r = (1-s)\omega_s.$$

Neglect core / frictional losses. $R_c = 0$, $P_{\text{friction}}^{\text{loss}} = 0$.

Rotor speed is 1720 ~~RPM~~
rotation per minute.

$$\therefore \omega_m = \frac{1720 \times 2\pi \text{ rad}}{60 \text{ s}} \left\{ \begin{array}{l} \text{why? } 1 \text{ rotation} = 2\pi \text{ rad} \\ 1 \text{ minute} = 60 \text{ s.} \end{array} \right.$$
$$= 180.1 \text{ rad/s.}$$

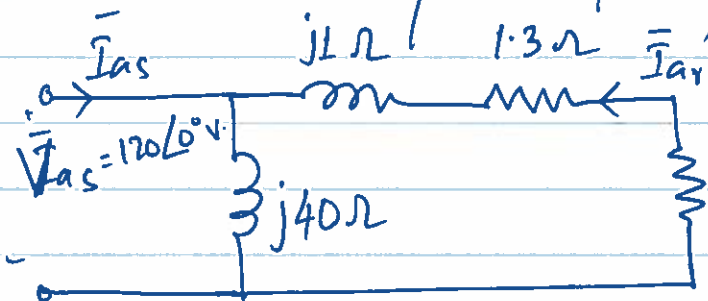
Let's embark on solving the problem now!

$$\begin{array}{l} \text{we know } \omega_s - \omega_r = \omega_m \cdot \frac{p}{2} \quad \text{we know } \Rightarrow \omega_r = \omega_s - \omega_m \cdot \frac{p}{2} \\ \text{we know } \end{array}$$
$$= 377 - 180.1 \times \frac{4}{2} \text{ rad/s}$$
$$= 16.8 \text{ rad/s.}$$

$$s\omega_s = \omega_r \Rightarrow s = \frac{\omega_r}{\omega_s} = \frac{16.8}{377} = 0.045$$

S has no units!

Now, let's draw equivalent circuit with the characteristic quantities as specified.



$$R_r' \left(\frac{1-s}{s} \right) = 1.3 \times \left(\frac{1-0.045}{0.045} \right) \Omega = 27.6 \Omega$$

$$\bar{I}_{ar}' = \frac{-\bar{V}_{as}}{j1\Omega + 1.3\Omega + 27.6\Omega}$$

$$\Rightarrow |\bar{I}_{ar}'| = \frac{120}{|j1 + 1.3 + 27.6|} \text{ Amps} = 4.1 \text{ Amps}$$

$$P_{mech}^{out} = P_{mech} = \text{power spent in } R_r' \left(\frac{1-s}{s} \right) = 3 \cdot \overbrace{|\bar{I}_{ar}'|^2}^{= 4.1 \text{ Amps}} \cdot \overbrace{R_r' \left(\frac{1-s}{s} \right)}^{= 27.6 \Omega} = 1.43 \text{ kW}$$

$$P_{airgap} = 3 \cdot |\bar{I}_{ar}'|^2 \cdot \frac{R_r'}{s} = 3 \times 4.1^2 \times \frac{1.3}{0.045} \text{ W} = 1.49 \text{ kW}$$

$$\bullet P_{3\phi}^{in} = \cancel{P_{stator}^{loss}} + \cancel{P_{core}^{loss}} + P_{airgap}.$$

$= 0 \quad (\because R_s = 0)$ $= 0 \text{ (given).}$

$$= P_{airgap} = 1.49 \text{ kW.}$$

$$\bullet T^e = \frac{P_{mech}}{\omega_m} = \frac{1.43 \text{ kW}}{180.1 \text{ rad/s}} = 7.94 \text{ N-m.}$$

$$\bullet \text{Efficiency} = \frac{P_{mech}^{out} \times 100\%}{P_{3\phi}^{in}} = \frac{1.43 \text{ kW}}{1.49 \text{ kW}} \times 100\%.$$

$$\approx 96\%.$$

Oh! We forgot to compute the power factor!

To do that, we need the angle of $\bar{I}_{as}$.

$$\bar{I}_{as} = \frac{\bar{V}_{as}}{Z_{eq}}, \text{ where } Z_{eq} = j40 \parallel (j1 + 1.3 + 27.6j)$$

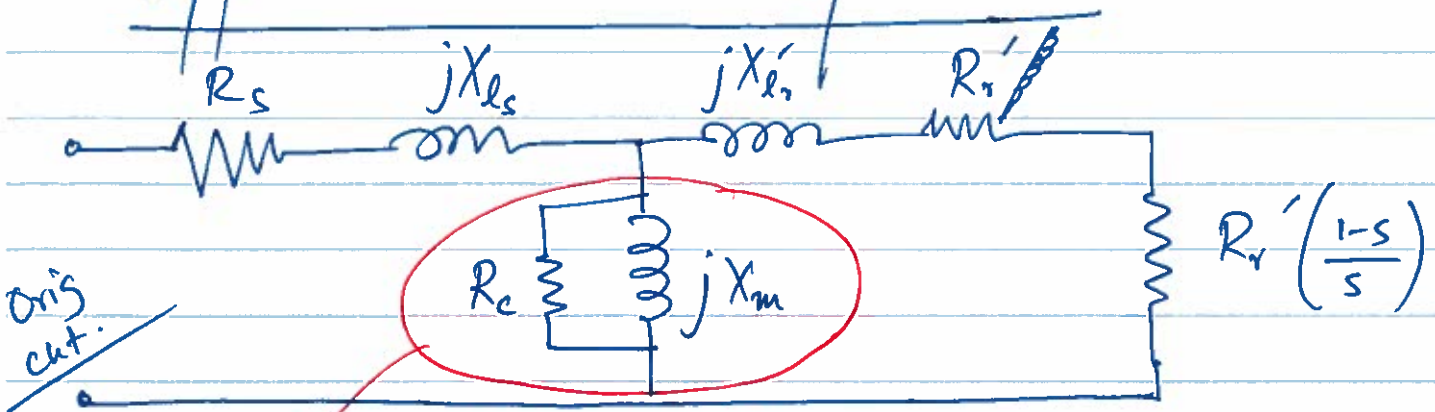
$$= (18.4 + j13.9) \Omega.$$

$$= 5.20 \angle -37.16^\circ.$$

$$\text{power-factor} = \cos(37.16^\circ) \approx 0.8 \text{ lagging.}$$

②

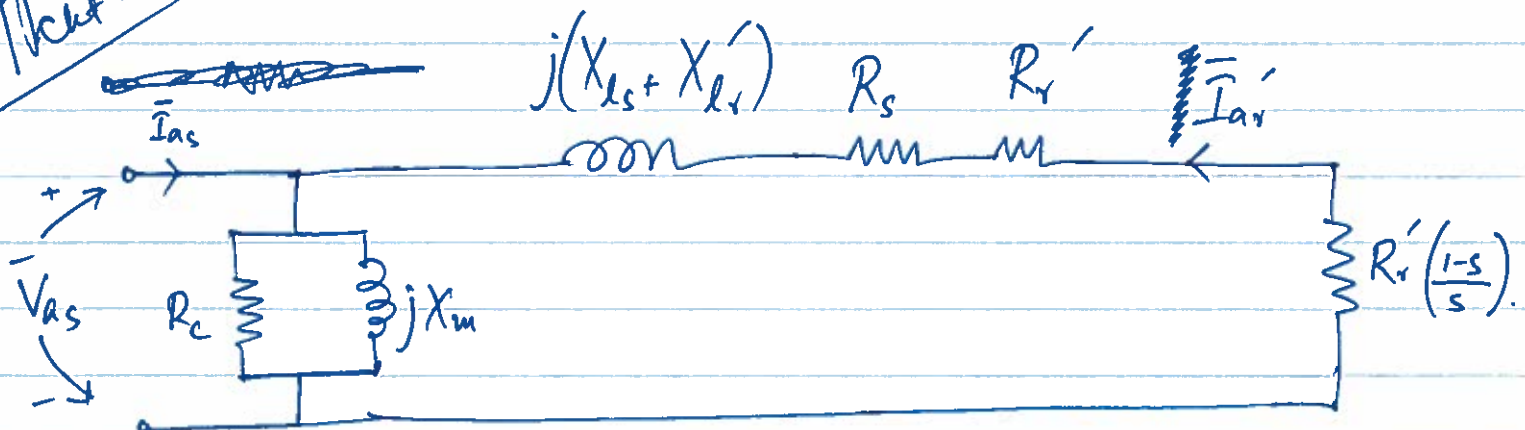
Approximate circuit equivalent



Remember the approx. ckt equivalent for a transformer?

Shift this block to the left of R_s, jX_{ls} .

Approx. ckt.

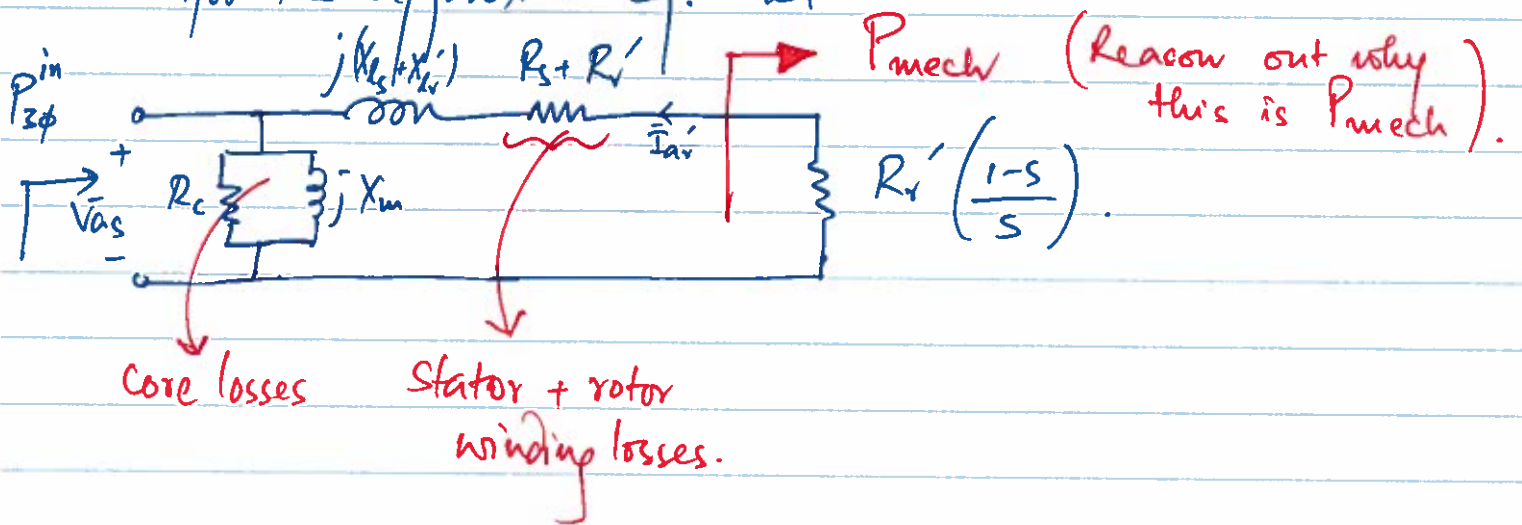


③ Torque-speed characteristics.

Q. How does T^e vary with slip? Sketch it!

Use the approximate equivalent circuit.

Solⁿ: Let's use our logic to deduce what T^e is for the approx. eq. ckt.



$$\begin{aligned}
 P_{mech} &= 3 \cdot |\bar{I}_{ar}'|^2 \cdot R_r' \left(\frac{1-s}{s} \right) \\
 &= 3 R_r' \left(\frac{1-s}{s} \right) \cdot \left| \frac{\bar{V}_{as}}{jX_s + jX_r' + R_s + R_r' + R_r' \left(\frac{1-s}{s} \right)} \right|^2
 \end{aligned}$$

write out $\bar{I}_{ar}$ in terms of $\bar{V}_{as}$ and impedances.

$$\begin{aligned}
 &\quad \underbrace{jX_s + jX_r'}_{:= jX} \quad \underbrace{R_s + R_r' + R_r' \left(\frac{1-s}{s} \right)}_{= R_s + \frac{R_r'}{s}} \\
 &= 3 R_r' \cdot \frac{1-s}{s} \cdot \frac{|\bar{V}_{as}|^2}{X^2 + \left(R_s + \frac{R_r'}{s} \right)^2}
 \end{aligned}$$

$$T^e = \frac{P_{\text{mech}}}{\omega_m}$$

$$\omega_s - \omega_r = \frac{p}{2} \omega_m$$

$$= s \omega_s$$

$$\Rightarrow \omega_m = (1-s) \omega_s \cdot \frac{2}{p}$$

$$= \frac{P_{\text{mech}}}{(1-s) \cdot \omega_s \cdot \frac{2}{p}}$$

$$= 3 \cdot R_r' \cdot \frac{1-s}{s} \cdot \frac{|\bar{V}_{as}|^2}{X^2 + \left(R_s + \frac{R_r'}{s}\right)^2} \cdot \frac{1}{(1-s) \cdot \omega_s \cdot \frac{2}{p}}$$

$$= \underbrace{\left(\frac{3p \cdot R_r' \cdot |\bar{V}_{as}|^2}{2 \omega_s} \right)}_{\text{const.}} \cdot \left(\frac{1}{s \left[X^2 + \left(R_s + \frac{R_r'}{s} \right)^2 \right]} \right)$$

Let's plot what this function looks like!

Use the following parameters:

$$p=4, \quad |\bar{V}_{as}| = 120, \quad \omega_s = 377 \text{ rad/s.}$$

$$X_{ls} = 0.01 \Omega, \quad X_{lr}' = 1 \Omega,$$

$$R_s = 0.01 \Omega, \quad R_r' = 1.3 \Omega.$$

Same values
as in the
example.

only these are
perturbed from the example.

Q. Can you find ~~the~~ the slip s for which $T^e(s)$ is max? Also, find $\max_{s \in \mathbb{R}} T^e(s)$.

~~Repeat~~ Repeat the entire process for ~~finding~~ finding where T^e is min.

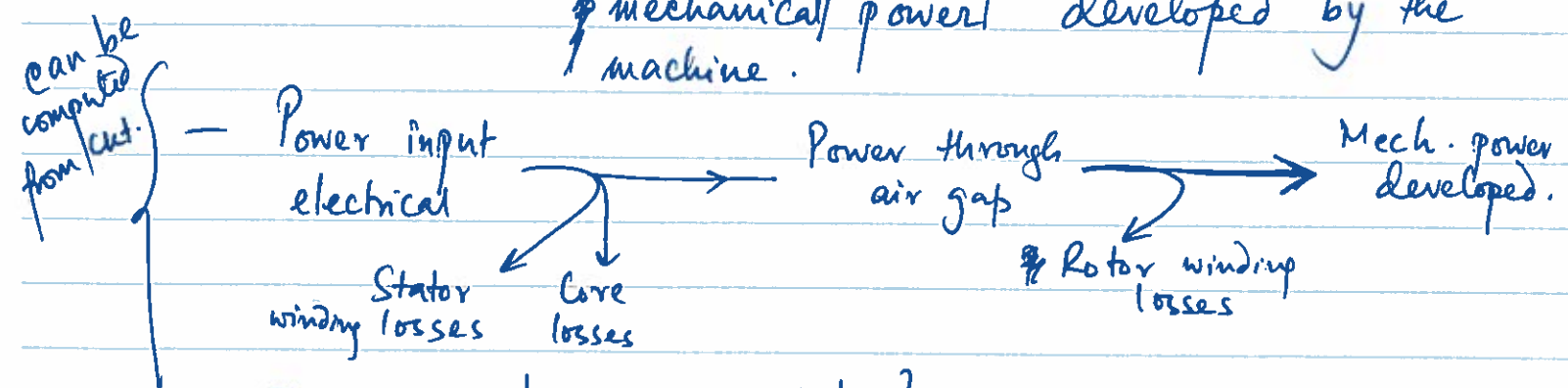
— We shall do this next class.

V.V. Imp.

Things to remember for induction machines.

- Equivalent circuit $\rightarrow$ approx. equiv. circuit.
- Power considerations.

— Remember: Circuit only computes P_{mech} , the mechanical power developed by the machine.



$$P_{mech} - P_{\text{loss friction}} = P_{\text{out mech}} \quad \left. \vphantom{P_{mech} - P_{\text{loss friction}}} \right\} \text{Useful output power.}$$

$$\omega_s - \omega_r = \frac{1}{2} \omega_m, \text{ and } \omega_r = s \omega_s.$$

$$T^e = P_{mech} / \omega_m.$$

Rest is manipulation!